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- (71) Applicant
  Halliburton Company
  PO Drawer 1431
  Duncan
  Oklahoma 73536
  United States of
  America
- (72) Inventors

  Jiten Chatterji

  Bobby Geral Brake
- (74) Agents
  A A Thornton & Co
  Northumberland House
  303–306 High Holborn
  London WC1V 7LE

## (54) Water loss reducing additives for salt water cement slurries

(57) Very low molecular weight carboxymethylhydroxyethylcellulose polymers are used as additives for salt water cement slurries to lower the water loss therefrom when in contact with water permeable earth formations. The additives may also include hydroxycarboxy acids. The cellulose derivative has a DS of 0.1-0.7 (carboxymethyl), a molar ratio of ethylene oxide to anhydroglucose units of 0.6-2.8 and a molecular weight such that a 1% by wt. aqueous solution at 25-5°C has a viscosity (FANN) of 10-225 cps at 300 rpm/no. 1 spring. Typical hydroxycarboxy acid additives include gluconic, tartaric, lactic, citric or malic acid.

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## **SPECIFICATION**

## Water loss reducing additives for salt water cement slurries

5	for carrying out cementing procedures such as cementing casings in the well bores, sealing subterranean zones penetrated by the well bores, etc. In most cases, the cement slurries are pumped into the well bores and allowed to harden once in place in the well bores or desired	5
10	A variety of additives have been developed and utilized heretofore for improving the properties of cement slurries and bringing about desired results including additives for reducing water loss from such slurries while or after the slurries are placed. Excessive water loss from cement slurries can prevent proper hydration of the cement, and in cementing wells, excessive water	10
15	slurries to the point where bridging of the cement and other solids takes place in the well bores preventing completion of cement displacement, etc. While the water loss reducing additives utilized heretofore are effective in cement slurries formed with fresh water or water containing very low concentrations of salts therein, such additives are substantially ineffective in cement	15
20	saturated with salts. For example, a number of cellulose derivatives have been utilized to control fluid loss from cement slurries containing little or no salts. However, such heretofore used cellulose derivatives are substantially ineffective in reducing water loss from salt water cement slurries. In addition, other heretofore used fresh water cement slurry water loss reducing	20
25	and poly-2-acrylamide-3-propylsulfonic acid salts are not effective in reducing water loss from salt water cement slurries.	25
30	are effective in reducing water loss from the slurries over a broad temperature range.  According to the invention, there is provided a water loss-reducing additive for use in salt water cement slurries, which additive comprises carboxymethylhydroxyethylcellulose having a carboxymethyl degree of substitution (D.S.) in the range 0.1 to 0.7, a molar ratio of ethylene oxide to anhydroglucose units (M.S.) of 0.6 to 2.8, and a molecular weight such that a 1% by	30
35	225 centipoises measured on a FANN viscometer at 300 rpm using a No. 1 spring.  The invention also provides a salt water cement slurry having low water loss when in contact with permeable earth formations, which comprises salt water; cement; and a water loss reducing	35
40	The invention further provides a method of reducing the water loss from a salt water cement slurry used in cementing a well, which comprises combining with said salt water cement slurry prior to using said slurry, a water loss reducing additive of the invention.  The term "salt water" is used herein to mean sea water, brines and other aqueous solutions	40
<b>45</b>	salt concentrations therein up to saturation. Salts other than those mentioned above can be tolerated in the cement slurries of this invention to some extent even though they may react with or alter the performance of the slurries, e.g. bicarbonates, phosphates and sulfates. The term "salt water cement slurry" is used herein to mean a cement slurry comprised of water, cement, one or more salts and other components or additives to bring about the desired slurry	45
50	expressed in percentages by weight of the water in the cement slurries. The amounts of water loss reducing additives in the cement slurries set forth hereinafter are expressed in percentages by weight of dry cement in the slurries.	50
	comprised of very low molecular weight carboxymethylhydroxyethylcellulose polymers. More specifically, the particular carboxymethylhydroxyethylcellulose polymers which are useful in	55
	10 15 20 25 30 40 45	subterranean zones penetrated by the well bores, etc. In most cases, the cement slurries are pumped into the well bores and allowed to harden once in place in the well bores or desired zones in formations.  A variety of additives have been developed and utilized heretofore for improving the properties of cement slurries and bringing about desired results including additives for reducing water loss from such slurries while or after the slurries are placed. Excessive water loss from cement slurries can prevent proper hydration of the cement, and in cementing wells, excessive water loss while the slurries are being flowed through well bores can result in dehydration of the slurries to the point where bridging of the cement and other solids takes place in the well bores preventing completion of cement displacement, etc. While the water loss reducing additives utilized herotofore are effective in cement slurries formed with fresh water or water containing very low concentrations of salts, and particularly, in cement slurries which are salurries containing high concentrations of salts, and particularly, in cement slurries which are cellulose derivatives are substantially ineffective in reducing water loss from salt water cement slurries. In addition, other heretofore used fresh water cement slurry water loss reducing additives, such as polyacrylamides, polyethylene imines mixed with naphthalene sulfonic acid and poly-2-acrylamides-3-propylsulfonic acid salts are not effective in reducing water loss from salt water cement slurries.  We have now found certain water loss reducing additives for salt water cement slurries, which are effective in reducing water loss from the slurries over a broad temperature range.  According to the invention, there is provided a water loss-reducing additive for use in salt over the reducing water loss from the slurries over a broad temperature range.  According to the invention, there is provided a water loss-reducing additive for use in salt acry weight such that a 1% by weight acuous so

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The portion of the above structural formula in brackets constitutes two anhydroglucose units, each having three reactive hydroxyl groups. n is an integer which gives the desired polymer molecular length. When the polymer is treated with sodium hydroxide and reacted with chloroacetic acid and ethylene oxide under controlled conditions, carboxymethylhydroxyethylcellulose is produced shown as follows:

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The sodium salt of carboxymethylhydroxyethylcellulose shown above has one of the side hydroxyl groups substituted by carboxymethyl, and therefore, the carboxymethyl degree of substitution (D.S) is 0.5 per anhydroglucose unit. As stated above, the preferred carboxymethyl degree of substitution for the carboxymethylhydroxyethylcellulose used in accordance with this invention is in the range of from about 0.1 to about 0.7. At a carboxymethyl D.S. of less than about 0.1, the carboxymethylhydroxyethylcellulose has limited solubility in water and at a carboxymethyl D.S. above about 0.7, the carboxymethylhydroxyethylcellulose has too much anionic characteristic and causes a precipitate to be formed when combined with a cement slurry.

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The above structural formula also shows that the ratio of moles of ethylene oxide to anhydroglucose unit (M.S.) is 1 mole for two units or 0.5. The preferred ethylene oxide M.S. for the carboxymethylhydroxyethylcellulose used in accordance with this invention is in the range of from about 0.6 to about 2.8. Carboxymethylhydroxyethylcellulose having an ethylene oxide M.S. outside the range given above does not give adequate water loss reducing properties to a salt water cement slurry.

The molecular length of the carboxymethylhydroxyethylcellulose polymers, i.e., the molecular

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While the carboxymethylhydroxyethylcellulose polymers described above are effective in reducing water loss from salt water cement slurries, when the concentration of salts in the slurries is above about 18% by weight of water, the effectiveness of the polymers by themselves decreases. However, when a hydroxycarboxy acid is combined with the carboxymethylhydroxye-thylcellulose polymers, the resulting additive is highly effective in reducing water loss from salt

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water cement slurries having high salt concentrations. More specifically, for salt water cement slurries having salt concentrations therein in the range of from about 18% by weight of water to saturation, an additive comprised of the carboxymethylhydroxyethylcellulose polymers described and a hydroxycarboxy acid present in the additive in an amount of about 50% of the weight of carboxymethylhydroxyethylcellulose in the additive is utilized. Particularly suitable hydroxycarboxy acids which can be used are gluconic acid, tartaric acid, lactic acid, citric acid, maleic acid and mixtures of such acids. Of these, gluconic acid, tartaric acid and citric acid are preferred with citric acid being the most preferred.

A preferred water loss reducing additive for salt water cement slurries having salt concentra-10 tions below about 18% by weight of the slurries is comprised of carboxymethylhydroxyethylcellulose having a carboxymethyl D.S. in the range of from about 0.1 to about 0.7, an ethylene oxide M.S. in the range of from about 0.6 to about 2.8 and a molecular weight such that a 1% by weight aqueous solution of the carboxymethylhydroxyethylcellulose at a temperature of 78°F has a viscosity in the range of from about 10 to about 225 centipoises measured on a FANN viscometer at 300 rpm using a No. 1 spring. The most preferred additive of this type is comprised of carboxymethylhydroxyethylcellulose having a carboxymethyl D.S. of about 0.4, an ethylene oxide M.S. of about 2.0 and a molecular weight wherein the viscosity of a 1% by weight aqueous solution is in the range of from about 10 to about 200.

A preferred water loss reducing additive for salt water cement slurries having salt concentra-20 tions therein in the range of from about 18% by weight of water to saturation is comprised of carboxymethylhydroxyethylcellulose having a carboxymethyl D.S. in the range of from about 0.1 to about 0.7, an ethylene oxide M.S. in the range of from about 0.6 to about 2.8, and a molecular weight such that a 1% by weight aqueous solution of said carboxymethylhydroxyethylcellulose at a temperature of 78°F has a viscosity in the range of from about 10 to about 25 225 centipoises measured on a FANN viscometer at 300 rpm using a No. 1 spring, and a hydroxycarboxy acid selected from the group consisting of gluconic acid, tartaric acid, lactic acid, citric acid, maleic acid and mixtures of such acids present in the additive in a weight amount of about 50% of the weight of carboxymethylhydroxyethylcellulose in the additive.

The most preferred additive of this type is comprised of carboxymethylhydroxyethylcellulose 30 having a carboxymethyl D.S. of about 0.4, an ethylene oxide M.S. of about 2.0 and a molecular 30 weight such that a 1% by weight aqueous solution thereof at a temperature of 25.5°C (78°F) has a viscosity in the range of from about 10 to about 200 centipoises measured on a FANN viscometer at 300 rpm using a No. 1 spring, and citric acid present in the additive in an amount of about 50% of the weight of carboxymethylhydroxyethylcellulose in the additive.

A preferred salt water cement slurry having low water loss when in contact with permeable earth formations of this invention is comprised of salt water, cement and a water loss reducing additive comprised of carboxymethylhydroxyethylcellulose having a carboxymethyl D.S. in the range of from about 0.1 to about 0.7, an ethylene oxide M.S. in the range of from about 0.6 to about 2.8 and a molecular weight such that a 1% by weight aqueous solution thereof at a 40 temperature of 25.5°C (78°F) has a viscosity in the range of from about 10 to about 225 centipoises measured on a FANN viscometer at 300 rpm using a No. 1 spring.

Another preferred salt water cement slurry having low water loss when in contact with permeable earth formations is comprised of salt water, cement, a water loss reducing additive comprised of carboxymethylhydroxyethylcellulose having a carboxymethyl D.S. in the range of 45 from about 0.1 to about 0.7, an ethylene oxide M.S. in the range of from about 0.6 to about 2.8 and a molecular weight such that a 1% by weight aqueous solution thereof at a temperature of 78°F has a viscosity in the range of from about 10 to about 225 centiposes measured on a FANN viscometer at 300 rpm using a No. 1 spring, present in the slurry in an amount in the range of from about 0.2% to about 2.0% by weight of dry cement in the slurry, and a 50 hydroxycarboxy acid selected from the group consisting of gluconic acid, tartaric acid, lactic acid, citric acid, maleic acid and mixtures of such acids present in said slurry in an amount in

the range of from about 0.1% to about 1.0% by weight of dry cement in the slurry. The most preferred salt water cement slurry having low water loss is comprised of salt water, cement, and a water loss reducing additive comprised of carboxymethylhydroxyethylcellulose 55 having a carboxymethyl D.S. of about 0.4, an ethylene oxide M.S. of about 2.0 and a molecular 55 weight such that a 1% by weight aqueous solution thereof at a temperature of 25.5°C (78°F) has a viscosity of from about 10 to about 200 centipoises measured on a FANN viscometer at 300 rpm using a No. 1 spring, the carboxymethylhydroxyethylcellulose being present in the

slurry in an amount in the range of from about 0.25% to about 1.8% by weight of dry cement 60 in the slurry and citric acid present in the slurry in an amount in the range of from about 0.1% to about 0.9% by weight of dry cement in the slurry.

In use of the water loss reducing additives of the present invention for reducing water loss from a salt water cement slurry used in cementing wells, the additive is combined with the salt water cement slurry prior to the use thereof. Preferably, the water loss reducing additive is dry

65 blended with other dry components and added to the mixing water used to prepare the cement

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slurry. If the mixing water does not already contain salts, the salt or salts used are preferably also dry blended with other dry components and the mixture then combined with the mixing water. Once the slurry is thoroughly mixed, it is introduced into a well bore and/or subterranean formations penetrated thereby and allowed to set into a hard permeable mass. The water loss 5 reducing additives and cement slurries including such additives are effective in substantially 5 reducing water loss at temperatures over a broad temperature range, i.e., from about 38°C (100°F) to about 182°C (360°F). As is well understood by those skilled in the art, the salt water cement slurries of this invention can include a variety of other components and additives to bring about desired results 10 including solid fillers such as sand, set time retarders, accelerators, etc. 10 In order that the invention may be more clearly understood, the following Examples are given by way of illustration only. Example 1 Cement slurries are prepared using fresh water containing various concentrations of sodium 15 chloride, cement and water loss reducing additives of this invention comprised of very low molecular weight carboxymethylhydroxyethylcellulose polymers (D.S. of 0.4, M.S. of 2.0, and a molecular weight such that a 1% by weight aqueous solution thereof at a temperature of 25.5°C (78°F) has a viscosity of from about 10 to about 200 centipoises measured on a FANN 20 viscometer at 300 rpm using a No. 1 spring) and tartaric acid. The slurries and additives are 20 mixed in a Waring Blender for 35 seconds at high speed. The surface mixing viscosities of the slurries are determined at 38°C (100°F), 43.5°C (120°F), 65°C (150°F) and 87.5°C (190°F) using a Halliburton consistometer as described in U.S. Patent No. 2,122,765. Fluid loss properties of the slurries are determined in accordance with API standard methods 25 (API RP-10B) on a 326 mesh screen at 70 kg/cm² (1000 psi) at 38°C (100°F), 43.5°C 25

(120°F), 65°C (150°F) and 87.5°C (190°F). The results of these tests are given in Table I below.

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TABLE I - PROPERTIES OF VARIOUS SALT WATER CENTRY SURRIES CONTAINING CARBOOMETHYLANDROMETHYLOEILLIJOSE (CHEC)-TARTARIC ACID WATER LOSS REDUCING ADITIVES

Trinity Class H         5.2         0.48         0.12         0           Trinity Class H         5.2         0.48         0.12         5           Trinity Class H         5.2         0.48         0.12         10           Trinity Class H         5.2         0.48         0.12         10           Trinity Class H         5.2         0.48         0.12         10           Trinity Class H         5.2         0.48         0.12         asturated           Trinity Class H         5.2         0.48         0.12         asturated           Trinity Class H         5.2         0.56         0.14         asturated           Trinity Class H         5.2         0.56         0.14         asturated           Trinity Class H         5.2         0.8         0.2         0           Trinity Class H         5.2         0.8         0.2         0           Lore Star Class H         5.2         0.8         0.2         0           Lore Star Class H         5.2         0.8         0.2         10           Lore Star Class H         5.2         0.8         0.2         2           Lore Star Class H         5.2         0.8         0.2	Quantity of Cement Quantity of CHECC Q in Slurry, Gallon in Slurry, 1 by A Water/Seck Meight Cement	Quantity of Turtaric Acid in Slurry, 1 by Weight Coment	Owantity of Nacl in Slurry, * by Neight Water	femperature of Slurry,	Initial Viscosity of Slurry, Be	Fluid Loss, cc/30 Min.
5.2     0.48     0.12       5.2     0.49     0.12       5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.49     0.12       8.2     0.49     0.12       8.2     0.40     0.12       8     5.2     0.14       8     5.2     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.6     0.2       8     5.2     0.2     0.2       8     5.2     0.2     0.2       8     5.2     0.2     0.2       8     5.2     0.2     0.2       8     5.2     0.2     0.2       8     5.2     0.2     0.2       9     0.2     0.2     0.2       9     0.2     0.2     0.2		0.12	0	38	•	=
5.2 0.48 0.12 5.2 0.48 0.12 5.2 0.48 0.12 5.2 0.48 0.12 5.2 0.48 0.12 5.2 0.48 0.12 5.2 0.48 0.12 6.2 0.48 0.12 6.2 0.48 0.12 6.2 0.48 0.12 6.3 0.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.48 0.12 6.49 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.40 0.12 6.		0.12	•	) (f	• •	) <b>4</b>
5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.56     0.14       H     5.2     0.8     0.2		0.12	2	: 27 66	• •	;
5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.46     0.12       5.2     0.56     0.14       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2		0.12	3 87	) e	• 60	3 3
5.2     0.48     0.12       5.2     0.48     0.12       5.2     0.46     0.12       5.2     0.56     0.14       8     5.2     0.0       8     5.2     0.6     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2       8     5.2     0.8     0.2		0.12	saturated	) & &	• 60	<b>3</b>
5.2     0.46     0.12       5.2     0.56     0.14       5.2     0.56     0.14       H     5.2     0.0     0.2       H     5.2     0.6     0.2       R     5.2     0.6     0.2	٠.	0.12	10	, e	y y	, <sub>2</sub>
5.2     0.56     0.14       5.2     0.56     0.14       8.2     0.8     0.2       H     5.2     0.8     0.2       Rater used as mixing vater     0.8     0.2		0.12	saturated	4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	) G	: y
5.2     0.56     0.14       8.2     0.8     0.2       8 5.2     0.8     0.2       8 5.2     0.8     0.2       8 5.2     0.8     0.2       8 5.2     0.8     0.2       8 5.2     0.8     0.2       8 5.2     0.8     0.2       8 5.2     0.8     0.2       A 5.2     0.8     0.2		0.14	ot	65,	, ,	3 2
H         5.2         0.8         0.2           R         5.2         0.8         0.2           Rather used as mixting vector         0.8         0.2		0.14	saturated	65	· v	<b>;</b> ;
H 5.2 0.6 0.2 H 5.2 0.8 0.2		0.3	•	87 F	· •	•
H 5.2 0.8 0.2 R 5.2 0.8 0.2		0.3	•	87.5	• •	: 5
H 5.2 0.8 0.2 H 5.2 0.8 0.2 H 5.2 0.8 0.2 H 5.2 0.8 0.2 At 5.2		0.2	· vn	87.5	•	<b>: :</b>
H 5.2 0.8 0.2 H 5.2 0.8 0.2 H 5.2 0.8 0.2 At 5.2		0.2	10	87.5	. თ	: 58
0.2		0.5	81	87.5	• •	; ;;
0.2		0.2	ĸ	87.5	• •	3
	•	. 2.0	saturated	87.5	•	; <b>#</b>
•					•	}
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From Table I it can be seen that the carboxymethylhydroxyethylcellulose-tartaric acid additives produce good surface mixing viscosities and fluid loss reduction in cement slurries containing various quantities of salts.

5 Example 2

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The procedure of Example 1 is repeated using water loss reducing additives comprised of the low molecular weight carboxymethylhydroxyethylcellulose polymers described and various hydroxycarboxy acids.

The results of these tests are given in Table II below.

THRIE II - PROPERCIES OF SALF WATER CONTAC SLIPRIES CONTACIONE VARIOUS WATER LOSS REDUCING ADDITIVES

	Weight Cement	200	Weight Cement	10 v ii ii ii ii ii	o O		OK / 33
Star	0			Weight Water		of Slurry, cp	
Star Star Star Star			0	0	38		9631
Star Star Star Star	4.0		• •		88	2.	700
Star	4.0	!	• •	• •	) &C	, ,	9 4
Star	4.0	1	• •	91	) «	•	8
	4.0	•	. 0	S 1	) (Y		9 6
	4.0	1	. 6		י מ י	<b>.</b>	971
Lone Star Class n	4.0	-	. 0	- Pararage	ວແ	. :	101
	7.0	citric	0.2		) ()	2 4	. 537
Lone Star Class II	4.0	citric	0.2	32	o oc	•	
Luie Star Class H	4.0	ctric	0.2	asturated.	o or	• •	9 5
Lone Star Class H	0.5				0 cc	• •	
Lone Star Class H	9.0	1	0	18	် က က		3 <b>4</b>
Lone Star Class H	0	-	•	•	65		9031
Star	9.0			•		2 -	3 5
Lone Star Class H	9.0		•	•		• ◄	2 7
Lone Star Class H	9.0	!	•	. 2	א ע ע	, 🛩	; ;
Line Star Class H	9.0	1	•	18		•	2
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Lone Star Class MZ	1.03	ettrte	0 2	SECUTACO			316
Lone Star Class H2	1.7	citric	0.2	BECHTSTOC		7.	<b>*</b>

Colculated values of fluid loss

15% by weight coarse sand included in slurry
1.0% by weight retarder included in slurry
41.2% by weight retarder included in slurry

5	From Table II it can be seen that good fluid loss reduction is obtained using the additives of this invention at temperatures of from 38°C (100°F) to 182°C (360°F). Further, it can be seen that additives including hydroxycarboxy acids are more effective in salt water cement slurries containing salt concentrations above about 18% by weight of water than those containing CMHEC alone.	5	
10	CLAIMS  1. A water loss-reducing additive for use in salt water cement slurries, which additive comprises carboxymethylhydroxyethylcellulose having a carboxymethyl degree of substitution (D.S.) in the range 0.1 to 0.7, a molar ratio of ethylene oxide to anhydroglucose units (M.S.) of 0.6 to 2.8, and a molecular weight such that a 1% by weight aqueous solution thereof at a temperature of 25.5°C (78°F) has a viscosity of from 10 to 225 centipoises measured on a	10	7
15	FANN viscometer at 300 rpm using a No. 1 spring.  2. An additive according to claim 1, wherein said carboxymethylhydroxyethylcellulose has a D.S. of 0.4, an M.S. of 2.0 and a molecular weight such that said viscosity is 10 to 200 centipoises.	15	
20	<ul> <li>3. An additive according to claim 1 or 2, which also includes a hydroxycarboxy acid.</li> <li>4. An additive according to claim 3, wherein said hydroxycarboxy acid is gluconic acid, tartaric acid, lactic acid, citric acid or maleic acid, or any mixture of two of more thereof.</li> <li>5. An additive according to claim 3 or 4, wherein said hydroxycarboxy acid is present in an amount of 50% of the weight of carboxymethylhydroxyethyl cellulose.</li> <li>6. A water-loss reducing additive according to claim 1 substantially as herein described in</li> </ul>	20	
25	either of the Examples.  7. A salt water cement slurry having low water loss when in contact with permeable earth formations, which comprises salt water; cement; and a water loss reducing additive as claimed in any of claims 1 to 6.	25	
30	8. A cement slurry according to claim 7, wherein the amount of carboxymethylhydroxyethylcellulose is from 0.2% to 2.0% by weight of dry cement.  9. A cement slurry according to claim 7 or 8, wherein the additive comprises a hydroxycarboxy acid which is present in the slurry in an amount of from 0.1% to 1.0% by weight of dry cement.	30	
35	10. A cement slurry according to claim 7 substantially as herein described in the Examples. 11. A method of reducing the water loss from a salt water cement slurry used in cementing a well, which comprises combining with said salt water cement slurry prior to using said slurry, a water loss reducing additive as claimed in any of claim 1 to 6. 12. A method according to claim 11, wherein the carboxymethylhydroxyethylcellulose is	35	
40	combined with said slurry in an amount of from 0.2% to 2.0% by weight of dry cement in said slurry, and wherein the additive includes a hydroxycarboxy acid which is present in an amount of from 0.1% to 1.0% by weight of dry cement in said slurry.  13. A method according to claim 11 substantially as herein described in the Examples.	40	

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